A3245

# Chopper-Stabilized Omnipolar Hall-Effect Switches 

## Features and Benefits

- Omnipolar operation
- Chopper stabilization
- Superior temperature stability
- Extremely low switchpoint drift
- Insensitive to physical stress
- Reverse battery protection
- Output short circuit protection
- Solid state reliability
- Small size
- Robust EMC capability
- High ESD ratings (HBM)


## Packages: 3 pin SOT23W (suffix LH), and 3 pin SIP (suffix UA)



## Description

The A3245 integrated circuit is an omnipolar, ultrasensitive Hall-effect switch with a digital output. This sensor has an integrated regulator permitting operation to 24 V , making it the first omnipolar switch available for operation to 24 V . This device is especially suited for operation over extended temperature ranges, up to $+150^{\circ} \mathrm{C}$. Superior high-temperature performance is made possible through an Allegro ${ }^{\circledR}$ patented dynamic offset cancellation, which reduces the residual offset voltage normally caused by device overmolding, temperature excursions, and thermal stress.

The A3245 Hall-effect switch includes the following on a single silicon chip: voltage regulator, Hall-voltage generator, smallsignal amplifier, chopper stabilization, Schmitt trigger, and a short circuit protected open-drain output. Advanced BiCMOS wafer fabrication processing is used to take advantage of lowvoltage requirements, component matching, very low inputoffset errors, and small component geometries.

The omnipolar operation of the A3245 allows activation with either a north or a south polarity field of sufficient strength. In the absence of a magnetic field, the output is off. This patented

Continued on the next page...

Not to scale

## Functional Block Diagram



## Description (continued)

magnetic-polarity-independence feature makes this device an excellent replacement for reed switches, with improved ease of manufacturing, because the A3245 does not require manufacturers to orient their magnets. These devices allow simple on/off switching in industrial, consumer, and automotive applications.

The A3245 is rated for operation between the ambient temperatures $-40^{\circ} \mathrm{C}$ and $85^{\circ} \mathrm{C}$ for the E temperature range, and $-40^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ for the L temperature range. The small geometries of the BiCMOS
process allow these devices to be provided in ultrasmall packages. The package styles available provide magnetically optimized solutions for most applications. Package LH is an SOT23W, a miniature low-profile surface-mount package, while package UA is a three-lead ultramini SIP for through-hole mounting. Each package is available in a lead $(\mathrm{Pb})$ free version, with $100 \%$ matte tin plated leadframes.

Selection Guide

| Part Number | Pb-Free $^{\mathbf{1}}$ | Packing $^{2}$ | Mounting | Ambient, $\mathbf{T}_{\mathbf{A}}$ <br> ( |
| :--- | :---: | :--- | :--- | :---: |
| A3245ELHLT-T | Yes | 7-in. reel, 3000 pieces/reel | 3-pin SOT23W surface mount | -40 to 85 |
| A3245EUA-T | Yes | Bulk, 500 pieces/bag | 3-pin SIP through hole |  |
| A3245LLHLT-T | Yes | 7-in. reel, 3000 pieces/reel | 3-pin SOT23W surface mount | -40 to 150 |
| A3245LUA-T | Yes | Bulk, 500 pieces/bag | 3-pin SIP through hole |  |

${ }^{1} \mathrm{~Pb}$-based variants are being phased out of the product line. Certain variants cited in this footnote are in production but have been determined to be NOT FOR NEW DESIGN. This classification indicates that sale of this device is currently restricted to existing customer applications. The device should not be purchased for new design applications because obsolescence in the near future is probable. Samples are no longer available. Status change: May 1, 2006. These variants include: A3245ELHLT, A3245EUA, A3245LLHT, and A3245LUA.
${ }^{2}$ Contact Allegro for additional packing options.

## Absolute Maximum Ratings

| Characteristic | Symbol | Notes | Rating | Units |
| :--- | :---: | :---: | :---: | :---: |
| Supply Voltage | $\mathrm{V}_{\mathrm{CC}}$ |  | 28 | V |
| Reverse-Supply Voltage | $\mathrm{V}_{\mathrm{RCC}}$ |  | -18 | V |
| Reverse-Supply Current | $\mathrm{I}_{\mathrm{RCC}}$ |  | -2 | mA |
| Output Off Voltage | $\mathrm{V}_{\mathrm{OUT}}$ |  | 28 | V |
| Output Current | $\mathrm{I}_{\mathrm{OUTSINK}}$ |  | Internally Limited | - |
| Magnetic Flux Density | B |  | Unlimited | G |
| Operating Ambient Temperature | $\mathrm{T}_{\mathrm{A}}$ | Range E | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |
|  |  | -40 to 150 | ${ }^{\circ} \mathrm{C}$ |  |
| Maximum Junction Temperature | $\mathrm{T}_{\mathrm{J}}(\max )$ |  | 165 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | $\mathrm{T}_{\text {stg }}$ |  | -65 to 170 | ${ }^{\circ} \mathrm{C}$ |

## Chopper-Stabilized Omnipolar Hall Effect Switches

OPERATING CHARACTERISTICS valid over full operating voltage and ambient temperature ranges, unless otherwise noted

| Characteristic | Symbol | Test Conditions | Min. | Typ. | Max. | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Electrical Characteristics |  |  |  |  |  |  |
| Supply Voltage ${ }^{1}$ | $\mathrm{V}_{\mathrm{CC}}$ | Operating, $\mathrm{T}_{\mathrm{J}}<165^{\circ} \mathrm{C}$ | 3.6 | - | 24 | V |
| Output Leakage Current | $\mathrm{l}_{\text {OUtoff }}$ | $\mathrm{V}_{\text {OUT }}=24 \mathrm{~V}, \mathrm{~B}<\mathrm{B}_{\mathrm{RP}}$ | - | - | 10 | $\mu \mathrm{A}$ |
| Output On Voltage | $\mathrm{V}_{\text {OUT(SAT) }}$ | $\mathrm{I}_{\text {OUT }}=20 \mathrm{~mA}, \mathrm{~B}>\mathrm{B}_{\text {OP }}$ | - | - | 500 | mV |
| Output Current Limit | $\mathrm{I}_{\text {OM }}$ | $\mathrm{B}>\mathrm{B}_{\mathrm{OP}}$ | 30 | - | 60 | mA |
| Power-On Time | $\mathrm{t}_{\mathrm{PO}}$ | $\mathrm{V}_{\mathrm{CC}}>\mathrm{V}_{\mathrm{CC}(\mathrm{MIN})}$ | - | - | 50 | $\mu \mathrm{s}$ |
| Chopping Frequency | $\mathrm{f}_{\mathrm{c}}$ |  | - | 200 | - | kHz |
| Output Rise Time ${ }^{2}$ | $\mathrm{t}_{\mathrm{r}}$ | $\mathrm{R}_{\text {LOAD }}=820 \Omega, \mathrm{C}_{\mathrm{S}}=20 \mathrm{pF}$ | - | - | 1 | $\mu \mathrm{s}$ |
| Output Fall Time ${ }^{2}$ | $\mathrm{t}_{\mathrm{f}}$ | $\mathrm{R}_{\text {LOAD }}=820 \Omega, \mathrm{C}_{\mathrm{S}}=20 \mathrm{pF}$ | - | - | 1 | $\mu \mathrm{s}$ |
| Supply Current | $\mathrm{I}_{\text {CCON }}$ | $\mathrm{B}>\mathrm{B}_{\mathrm{OP}}$ | - | 1.5 | 3.5 | mA |
|  | $\mathrm{I}_{\text {CCOFF }}$ | $\mathrm{B}<\mathrm{B}_{\mathrm{RP}}$ | - | 1.5 | 3.5 | mA |
| Reverse Battery Current | $\mathrm{I}_{\mathrm{RCC}}$ | $\mathrm{V}_{\mathrm{RCC}}=-18 \mathrm{~V}$ | - | - | -2 | mA |
| Supply Zener Clamp Voltage | $\mathrm{V}_{\text {ZSupply }}$ | $\mathrm{I}_{\mathrm{CC}}=6.5 \mathrm{~mA} ; \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 28 | - | - | V |
| Supply Zener Current ${ }^{3}$ | İSupply | $\mathrm{V}_{\mathrm{S}}=28 \mathrm{~V}$ | - | - | 6.5 | mA |
| Magnetic Characteristics ${ }^{4}$ |  |  |  |  |  |  |
| Operate Point | $\mathrm{B}_{\text {OPS }}$ | South pole adjacent to branded face of device | 15 | 38 | 55 | G |
|  | $\mathrm{B}_{\text {OPN }}$ | North pole adjacent to branded face of device | -55 | -38 | -15 | G |
| Release Point | $\mathrm{B}_{\text {RPS }}$ | South pole adjacent to branded face of device | 5 | 20 | 50 | G |
|  | $\mathrm{B}_{\text {RPN }}$ | North pole adjacent to branded face of device | -50 | -20 | -5 | G |
| Hysteresis | $\mathrm{B}_{\mathrm{HYS}}$ | $\left\|\mathrm{B}_{\mathrm{OPX}}-\mathrm{B}_{\mathrm{RPX}}\right\|$ | 5 | 18 | 30 | G |

${ }^{1}$ Maximum voltage must be adjusted for power dissipation and junction temperature, see Power Derating section.
${ }^{2} \mathrm{C}_{S}=$ oscilloscope probe capacitance.
${ }^{3}$ Maximum current limit is equal to the maximum $\mathrm{I}_{\mathrm{CC}(\mathrm{MAX})}+3 \mathrm{~mA}$.
${ }^{4}$ Magnetic flux density, B, is indicated as a negative value for north-polarity magnetic fields, and as a positive value for south-polarity magnetic fields. This so-called algebraic convention supports arithmetic comparison of north and south polarity values, where the relative strength of the field is indicated by the absolute value of $B$, and the sign indicates the polarity of the field (for example, a - 100 G field and a 100 G field have equivalent strength, but opposite polarity).

## DEVICE QUALIFICATION PROGRAM <br> Contact Allegro for information.

EMC (Electromagnetic Compatibility) REQUIREMENTS
Contact Allegro for information.

# Chopper-Stabilized Omnipolar Hall Effect Switches 

## Electrical Characteristic Data








A3245

## Chopper-Stabilized Omnipolar Hall Effect Switches

## Magnetic Characteristic Data







Continued on the next page...

A3245

# Chopper-Stabilized Omnipolar Hall Effect Switches 

## Magnetic Characteristic Data (Continued)







# Chopper-Stabilized Omnipolar Hall Effect Switches 

THERMAL CHARACTERISTICS may require derating at maximum conditions, see application information

| Characteristic | Symbol | Test Conditions | Value | Units |
| :---: | :---: | :--- | :---: | :---: |
| Package Thermal Resistance | R | Package LH-3, 1-layer PCB with copper limited to <br> solder pads | 110 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  |  | 228 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |
|  | Package UA, 1-layer PCB with copper limited to <br> solder pads | 165 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |

## Power Derating Curve



Power Dissipation versus Ambient Temperature


# Chopper-Stabilized Omnipolar Hall Effect Switches 

## Functional Description

## Operation

The output of this device switches low (turns on) when a magnetic field perpendicular to the Hall sensor exceeds the operate point, $\mathrm{B}_{\text {OPS }}$ (or is less than $\mathrm{B}_{\text {OPN }}$ ). After turn-on, the output voltage is $\mathrm{V}_{\mathrm{OUT}(\mathrm{SAT})}$. The output transistor is capable of sinking current up to the short circuit current limit, $\mathrm{I}_{\mathrm{OM}}$, which is a minimum of 30 mA . When the magnetic field is reduced below the release point, $\mathrm{B}_{\text {RPS }}$ (or increased above $\mathrm{B}_{\text {RPN }}$ ), the device output switches high (turns off). The difference in the magnetic operate and release points is the hysteresis, $\mathrm{B}_{\mathrm{HYS}}$, of the device. This built-in hysteresis allows clean switching of the output even in the presence of external mechanical vibration and electrical noise.

Powering-on the device in a hysteresis region, between $\mathrm{B}_{\mathrm{OPX}}$ and $\mathrm{B}_{\text {RPX }}$, allows an indeterminate output state. The correct state is attained after the first excursion beyond $\mathrm{B}_{\mathrm{OPX}}$ or $\mathrm{B}_{\mathrm{RPX}}$.

## Applications

It is strongly recommended that an external bypass capacitor be connected (in close proximity to the Hall sensor) between the
supply and ground of the device to reduce both external noise and noise generated by the chopper stabilization technique. As is shown in Panel B of figure 1, a $0.1 \mu \mathrm{~F}$ capacitor is typical.

Omnipolar switches allow operation with either a north pole or south pole magnet orientation, enhancing product manufacturability with the device.

Extensive applications information on magnets and Hall-effect sensors is available in:

- Hall-Effect IC Applications Guide, AN27701,
- Hall-Effect Devices: Gluing, Potting, Encapsulating, Lead Welding and Lead Forming, AN27703.1
- Soldering Methods for Allegro's Products - SMT and ThroughHole, AN26009

All are provided in Allegro Electronic Data Book, AMS-702 and the Allegro Web site: www.allegromicro.com


Figure 1: Switching Behavior of Omnipolar Switches. In Panel A, on the horizontal axis, the B+ direction indicates increasing south polarity magnetic field strength, and the $B$-direction indicates decreasing south polarity field strength (including the case of increasing north polarity). This behavior can be exhibited when using a circuit such as that shown in panel B.

# Chopper-Stabilized Omnipolar Hall Effect Switches 

## Chopper Stabilization Technique

When using Hall-effect technology, a limiting factor for switchpoint accuracy is the small signal voltage developed across the Hall element. This voltage is disproportionally small relative to the offset that can be produced at the output of the Hall sensor. This makes it difficult to process the signal while maintaining an accurate, reliable output over the specified operating temperature and voltage ranges.

Chopper stabilization is a unique approach used to minimize Hall offset on the chip. The patented Allegro technique, namely Dynamic Quadrature Offset Cancellation, removes key sources of the output drift induced by thermal and mechanical stresses. This offset reduction technique is based on a signal modulationdemodulation process. The undesired offset signal is separated from the magnetic-field-induced signal in the frequency domain, through modulation. The subsequent demodulation acts as a modulation process for the offset, causing the magnetic-fieldinduced signal to recover its original spectrum at baseband, while the dc offset becomes a high-frequency signal. The mag-netic-field-induced signal then can pass through a low-pass filter, while the modulated dc offset is suppressed. This configuration is illustrated in figure 2.

The chopper stabilization technique uses a 200 kHz high-frequency clock. For demodulation process, a sample and hold technique is used, where the sampling is performed at twice the chopper frequency ( 400 kHz ). This high-frequency operation allows a greater sampling rate, which results in higher accuracy and faster signal-processing capability. This approach desensitizes the chip to the effects of thermal and mechanical stresses, and produces devices that have extremely stable quiescent Hall output voltages and precise recoverability after temperature cycling. This technique is made possible through the use of a BiCMOS process, which allows the use of low-offset, low-noise amplifiers in combination with high-density logic integration and sample-and-hold circuits.

The repeatability of magnetic-field-induced switching is affected slightly by a chopper technique. However, the Allegro highfrequency chopping approach minimizes the affect of jitter and makes it imperceptible in most applications. Applications that are more likely to be sensitive to such degradation are those requiring precise sensing of alternating magnetic fields; for example, speed sensing of ring-magnet targets. For such applications, Allegro recommends its digital sensor families with lower sensitivity to jitter. For more information on those devices, contact your Allegro sales representative.


Figure 2. Chopper Stabilization Circuit (Dynamic Quadrature Offset Cancellation)

## Chopper-Stabilized Omnipolar Hall Effect Switches

## Power Derating

The device must be operated below the maximum junction temperature of the device, $\mathrm{T}_{\mathrm{J}(\max )}$. Under certain combinations of peak conditions, reliable operation may require derating supplied power or improving the heat dissipation properties of the application. This section presents a procedure for correlating factors affecting operating $\mathrm{T}_{\mathrm{J}}$. (Thermal data is also available on the Allegro MicroSystems Web site.)
The Package Thermal Resistance, $\mathrm{R}_{\theta \mathrm{JA}}$, is a figure of merit summarizing the ability of the application and the device to dissipate heat from the junction (die), through all paths to the ambient air. Its primary component is the Effective Thermal Conductivity, K , of the printed circuit board, including adjacent devices and traces. Radiation from the die through the device case, $R_{\theta \mathrm{JC}}$, is relatively small component of $\mathrm{R}_{\theta \mathrm{JA}}$. Ambient air temperature, $\mathrm{T}_{\mathrm{A}}$, and air motion are significant external factors, damped by overmolding.

The effect of varying power levels (Power Dissipation, $\mathrm{P}_{\mathrm{D}}$ ), can be estimated. The following formulas represent the fundamental relationships used to estimate $T_{\mathrm{J}}$, at $\mathrm{P}_{\mathrm{D}}$.

$$
\begin{gather*}
\mathrm{P}_{\mathrm{D}}=\mathrm{V}_{\mathrm{IN}} \times \mathrm{I}_{\mathrm{IN}}  \tag{1}\\
\Delta \mathrm{~T}=\mathrm{P}_{\mathrm{D}} \times \mathrm{R}_{\theta \mathrm{JA}}  \tag{2}\\
\mathrm{~T}_{\mathrm{J}}=\mathrm{T}_{\mathrm{A}}+\Delta \mathrm{T} \tag{3}
\end{gather*}
$$

For example, given common conditions such as: $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, $\mathrm{V}_{\mathrm{CC}}=12 \mathrm{~V}, \mathrm{I}_{\mathrm{CC}}=1.5 \mathrm{~mA}$, and $\mathrm{R}_{\theta \mathrm{JA}}=165^{\circ} \mathrm{C} / \mathrm{W}$, then:

$$
\begin{aligned}
& \mathrm{P}_{\mathrm{D}}=\mathrm{V}_{\mathrm{CC}} \times \mathrm{I}_{\mathrm{CC}}=12 \mathrm{~V} \times 1.5 \mathrm{~mA}=18 \mathrm{~mW} \\
& \Delta \mathrm{~T}=\mathrm{P}_{\mathrm{D}} \times \mathrm{R}_{\theta \mathrm{JA}}=18 \mathrm{~mW} \times 165^{\circ} \mathrm{C} / \mathrm{W}=3^{\circ} \mathrm{C}
\end{aligned}
$$

$$
\mathrm{T}_{\mathrm{J}}=\mathrm{T}_{\mathrm{A}}+\Delta \mathrm{T}=25^{\circ} \mathrm{C}+3^{\circ} \mathrm{C}=28^{\circ} \mathrm{C}
$$

A worst-case estimate, $\mathrm{P}_{\mathrm{D}(\max )}$, represents the maximum allowable power level $\left(\mathrm{V}_{\mathrm{CC}(\max )}, \mathrm{I}_{\mathrm{CC}(\max )}\right)$, without exceeding $\mathrm{T}_{\mathrm{J}(\max )}$, at a selected $\mathrm{R}_{\theta \mathrm{JA}}$ and $\mathrm{T}_{\mathrm{A}}$.

Example: Reliability for $\mathrm{V}_{\mathrm{CC}}$ at $\mathrm{T}_{\mathrm{A}}=150^{\circ} \mathrm{C}$, package LH , using a low-K PCB.

Observe the worst-case ratings for the device, specifically:
$\mathrm{R}_{\theta \mathrm{JA}}=228^{\circ} \mathrm{C} / \mathrm{W}, \mathrm{T}_{\mathrm{J}(\max )}=165^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{CC}(\max )}=24 \mathrm{~V}$, and
$\mathrm{I}_{\mathrm{CC}(\max )}=5 \mathrm{~mA}$.
Calculate the maximum allowable power level, $\mathrm{P}_{\mathrm{D}(\max )}$. First, invert equation 3 :

$$
\Delta \mathrm{T}_{\max }=\mathrm{T}_{\mathrm{J}(\max )}-\mathrm{T}_{\mathrm{A}}=165^{\circ} \mathrm{C}-150^{\circ} \mathrm{C}=15^{\circ} \mathrm{C}
$$

This provides the allowable increase to $\mathrm{T}_{\mathrm{J}}$ resulting from internal power dissipation. Then, invert equation 2 :

$$
\mathrm{P}_{\mathrm{D}(\max )}=\Delta \mathrm{T}_{\max } \div \mathrm{R}_{\theta \mathrm{JA}}=15^{\circ} \mathrm{C} \div 228^{\circ} \mathrm{C} / \mathrm{W}=65.8 \mathrm{~mW}
$$

Finally, invert equation 1 with respect to voltage:

$$
\mathrm{V}_{\mathrm{CC}(\text { est })}=\mathrm{P}_{\mathrm{D}(\max )} \div \mathrm{I}_{\mathrm{CC}(\max )}=65.8 \mathrm{~mW} \div 5 \mathrm{~mA}=13.2 \mathrm{~V}
$$

The result indicates that, at $\mathrm{T}_{\mathrm{A}}$, the application and device can dissipate adequate amounts of heat at voltages $\leq \mathrm{V}_{\mathrm{CC} \text { (est) }}$.

Compare $\mathrm{V}_{\mathrm{CC}(\text { est })}$ to $\mathrm{V}_{\mathrm{CC}(\max )}$. If $\mathrm{V}_{\mathrm{CC}(\text { est })} \leq \mathrm{V}_{\mathrm{CC}(\max )}$, then reliable operation between $\mathrm{V}_{\mathrm{CC}(\text { est })}$ and $\mathrm{V}_{\mathrm{CC}(\max )}$ requires enhanced $\mathrm{R}_{\theta \mathrm{JA}}$. If $\mathrm{V}_{\mathrm{CC}(\text { est })} \geq \mathrm{V}_{\mathrm{CC}(\max )}$, then operation between $\mathrm{V}_{\mathrm{CC}(\text { est })}$ and $\mathrm{V}_{\mathrm{CC}(\max )}$ is reliable under these conditions.

# Chopper-Stabilized Omnipolar Hall Effect Switches 

Package LH, 3-Pin (SOT-23W)

Preliminary dimensions, for reference only
Dimensions in millimeters
U.S. Customary dimensions (in.) in brackets, for reference only
(reference JEDEC TO-236 AB, except case width and terminal tip-to-tip)
Dimensions exclusive of mold flash, gate burrs, and dambar protrusions Exact case and lead configuration at supplier discretion within limits shown
A) Hall element (not to scale)

BActive Area Depth 0.28 [.011]


Package LH


Package UA


Terminal List

| Name | Description | Number |  |
| :---: | :--- | :---: | :---: |
|  |  | Package LH | Package UA |
| VCC | Connects power supply to chip | 1 | 1 |
| VOUT | Output from circuit | 2 | 3 |
| GND | Ground | 3 | 2 |

Package UA, 3-Pin SIP


The products described herein are manufactured under one or more of the following U.S. patents: 5,045,920; 5,264,783; 5,442,283; 5,389,889; 5,581,179; 5,517,112; 5,619,137; 5,621,319; 5,650,719; 5,686,894; 5,694,038; 5,729,130; 5,917,320; and other patents pending.

Allegro MicroSystems, Inc. reserves the right to make, from time to time, such departures from the detail specifications as may be required to permit improvements in the performance, reliability, or manufacturability of its products. Before placing an order, the user is cautioned to verify that the information being relied upon is current.

Allegro products are not authorized for use as critical components in life-support devices or systems without express written approval.
The information included herein is believed to be accurate and reliable. However, Allegro MicroSystems, Inc. assumes no responsibility for its use; nor for any infringement of patents or other rights of third parties which may result from its use.

Copyright © 2005, 2006 Allegro MicroSystems, Inc.

