Application Specific Discretes A.S.D ${ }^{\text {TM }}$

OVERVOLTAGE \& OVERCURRENT PROTECTION FOR TELECOM LINE

## MAIN APPLICATIONS

Any telecom equipment submitted to transient overvoltages and lightning strikes such as :

- Analog and ISDN line cards
- PABX


## DESCRIPTION

The CLP30-200B1 is designed to protect telecommunication equipment. It provides both a transient overvoltage protection and an overcurrent protection.
The external components (balanced resistors, ring relays contact, ...) needed by the CLP30-200B1 protection concept require very low power rating. This results in a very cost effective protection solution.

## FEATURES

- Dual bidirectional protection device.
- High peak pulse current :

IPP $=40 \mathrm{~A}(5 / 310 \mu \mathrm{~s}$ SURGE)
IPP = 30A (10/1000 $\mu$ s SURGE)

- Max. voltage at switching-on : 290V
- Min. current at switching-off : 150mA


## BENEFITS

- Voltage and current controlled suppression.
- Surface Mounting with SO8 package.
- Very low power rating of external components on line card : balanced resistors, ring relay, low voltage SLIC protection.


SCHEMATIC DIAGRAM (Top view)


CLP30-200B1

| Standard | Peak surge <br> voltage <br> (V) | Voltage <br> waveform | Required peak <br> current (A) | Current <br> waveform | Minimum <br> serial resistor to <br> meet <br> standard $(\Omega)$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Bellcore TR-NWT-1089 <br> First level | 2500 <br> 1000 | $2 / 10 \mu \mathrm{~s}$ <br> $10 / 100 \mu \mathrm{~s}$ | 500 <br> 100 | $2 / 10 \mu \mathrm{~s}$ <br> $10 / 1000 \mu \mathrm{~s}$ | 20 <br> 25 |
| Bellcore TR-NWT-1089 <br> Second level | 5000 | $2 / 10 \mu \mathrm{~s}$ | 500 | $2 / 10 \mu \mathrm{~s}$ | 40 |
| ITU-T-K20 / K21 | 4000 | $10 / 700 \mu \mathrm{~s}$ | 100 | $5 / 310 \mu \mathrm{~s}$ | 50 |
|  | 1000 |  | 25 |  | 0 |
| ITU-T-K20 | 6000 | $1 / 60 \mathrm{~ns}$ | ESD contact discharge <br> ESD air discharge | 0 <br> (IEC61000-4-2) | 8000 |

## BLOCK DIAGRAM



| Pin | Symbol | Description |
| :---: | :---: | :---: |
| 1 | TIPL | TIP (Line side) |
| $2 / 3 / 6 / 7$ | GND | Ground |
| 4 | RINGL | RING (Line side) |
| 5 | RINGS | RING (SLIC side) |
| 8 | TIPS | TIP (SLIC side) |

## APPLICATION NOTE

## 1.INTRODUCTION

The aim of this section is to show the behavior of our new telecom line protection device.

Fig. 1 : Suscriber line protection topology


Figure 1 is a simplified block diagram of a subscriber line protection that is mainly used so far.
This shows two different things :

- A "primary protection" located on the Main Distribution Frame (MDF) eliminates coarsely the high energy environmental disturbances (lightning transients and AC power mains disturbances) for which the ITU-T-K20 requires a 4 kV $10 / 700 \mu$ s test. This can be assumed either by gas-tubes or silicon protection such as the TLPxxM.
- A "secondary protection" located on the line card eliminates finely the remaining transients that have not been totally suppressed by the first stage. The ITU-T-K20 requires a 1 kV $10 / 700 \mu$ s test. At this stage, the protection is managed by the CLP30-200B1.


## 2. STMicroelectronics CLP30-200B1 CONCEPT

### 2.1 Evolution of the SLIC protection

Over the years, the performances of the SLICs considerably increased and therefore the need of the protection has also evolved.
The CLP30-200B1 is especially designed for the protection of this new generation of SLIC. For this, it is based on both overvoltage and overcurrent protection modes.

Fig. 2 : Line card protection


The figure 2 summarises the performance of the CLP30-200B1 which basically holds the SLIC inside its correct voltage and current values.

## CLP30-200B1

## APPLICATION CIRCUIT : CLP30-200B1 in line card

Fig. 3 : CLP30-200B1 in line card


Figure above shows the topology of a protected analog subscriber line at the line card side.

- A first stage based on CLP30-200B1 manages the high power issued from the external surges. When used in ringing mode, the CLP30-200B1 operates in voltage mode and provides a symmetrical and bidirectional overvoltage protection above 200 V on both TIP and RING lines. When used in speech mode, the CLP30-200B1 operates in current mode and the activation current of the CLP30-200B1 is adjusted by RsEnse.
- A second stage which is the external voltage reference device defines the firing threshold voltage during the speech mode and also assumes a residual power overvoltage suppression. This stage can be either a fixed or programmable device such as LCP1511D.


### 2.3 Ringing mode

Fig. 4 : Switching by voltage during ringing mode.


In ringing mode (Ring relay in position 2), the only protection device involved is the CLP30-200B1.
In normal conditions, the CLP30-200B1 operates in region 1 of A1 curve, and is idle.
If an overvoltage occurring between TIP (or RING) and GND reaches the internal overvoltage reference (+/-200V), the CLP30-200B1 acts and the line is short-circuited to GND. At this time the operating point moves to region 2 for positive surges (region 3 for negative surges). Once the surge current disappears, the device returns to its initial state (region 1).

For surges occurring between TIP and RING, the CLP30-200B1 acts in the same way. This means that the CLP30-200B1 ensures a tripolar protection.

When used alone, the CLP30-200B1 acts at the internal overvoltage reference level (+/- 200 V ). Furthermore, it is possible to adjust this threshold level to a lower voltage by using up to 4 fixed external voltage reference $\left(\mathrm{V}_{\mathrm{Z1}}\right.$ to $\left.\mathrm{V}_{\mathrm{Z} 4}\right)$ (see fig.5).

Fig. 5 : Methode to adjust the reference voltage.


## CLP30-200B1

### 2.4 Speech mode

Fig. 6 : Switching by current during speech mode.


In speech mode (Ring relay in position 1), the protection is provided by the combination of both CLP30-200B1 and the external voltage reference device (for example LCP1511D).
In normal conditions, the working point of this circuit is located in region 4 of A2 curve : the CLP30-200B1 is idle.
When a surge occurs on the line, the external voltage reference device clamps at GND or $-\mathrm{V}_{\text {bat }}$ respectively for positive and negative surges. This generates a current which is detected by RSENSE and causes the protection to act : the line is short-circuited to GND. The operating point moves to region 6 for positive surges or region 5 for negative surges.

Once the surge current falls below the switching-off current Iswoff, the CLP30-200B1 returns to its initial state (region 4).

Furthermore, the CLP30-200B1 switches when an overvoltage, either positive or negative, occurs either:

- simultaneously on both TIP and RING lines versus GND.
- between TIP and RING.
- on TIP (or RING) versus GND.

The choice of the switching-on current is function of the RSENSE resistors.

Fig. 7a and 7b : Switching-on current versus RsEnSE


This current (typically above 150 mA ) should not activate the protection device CLP30-200B1.
Therefore the level of activation is to be chosen just below this limit (typically 200mA). This level is adjusted through RSENSE.
Figures 7a and 7b enable the designers to choose the right RSENSE value.
Example: The choice of $\mathbf{R}_{\text {SENSE }}=3 \Omega$ ensures a negative triggering of -280 mA min and -380 mA max. In this case, the positive triggering will be 220 mA min and 320 mA max.

Thanks to the CLP30-200B1 topology, the surge current in the line is reduced after it.
Because the remaining surge energy is low, the power ratings of $R_{P}$, the relay contacts and the external voltage reference device may be kept low. This results in a significant cost reduction for the whole system.

ABSOLUTE MAXIMUM RATINGS (RSENSE $=3 \Omega, \mathrm{~T}_{\text {amb }}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{I}_{\mathrm{PP}}$ | Line to GND peak pulse current |  |  |
|  | $10 / 1000 \mu \mathrm{~s}$ (open circuit voltage wave shape $10 / 1000 \mu \mathrm{~s}$ ) | 30 | A |
|  | $5 / 310 \mu \mathrm{~s}$ (open circuit voltage wave shape $10 / 700 \mu \mathrm{~s})$ | 45 |  |
| $\mathrm{I}_{\mathrm{TSM}}$ | Non repetitive surge peak on-state current | $\mathrm{t}_{\mathrm{p}}=10 \mathrm{~ms}$ | 8.5 |
|  | $\mathrm{~F}=50 \mathrm{~Hz}$ | $\mathrm{t}_{\mathrm{p}}=200 \mathrm{~ms}$ | 4.5 |
|  |  | $\mathrm{t}_{\mathrm{p}}=1 \mathrm{~s}$ | 3.5 |
| $\mathrm{~T}_{\text {stg }}$ | Storage temperature range | -40 to +150 | ${ }^{\circ}{ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{j}}$ | Maximum junction temperature | 150 |  |
| $\mathrm{~T}_{\mathrm{L}}$ | Lead temperature for soldering during 10 s. | 260 | ${ }^{\circ} \mathrm{C}$ |

ELECTRICAL CHARACTERISTICS (RSENSE $=3 \Omega$, and $\mathrm{T}_{\text {amb }}=25^{\circ} \mathrm{C}$ )

| Symbol | Parameter | Test condtions | Min | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ILgl | Line to GND leakage current | VLG $=200 \mathrm{~V}$ <br> Measured between TIP (or RING) and GND |  | 10 | $\mu \mathrm{A}$ |
| VLG | Line to GND operating voltage |  | 200 |  | V |
| Vswon | Line to GND voltage at SW1 or SW2 switching-on | Measured at 50 Hz between TIPL (or RINGL) and GND, one cycle |  | 290 | V |
| Iswoff | Line to GND negative current at SW1 or SW2 switching-off | Refer to test circuit fig 9 | 150 |  | mA |
| Iswon | Line current at SW1 or SW2 switching-on | Positive surge Negative surge | $\begin{aligned} & 220 \\ & 370 \end{aligned}$ | $\begin{aligned} & 320 \\ & 470 \end{aligned}$ | mA |
| c | Line to GND capacitance | $\begin{aligned} & V_{\mathrm{LG}}=0 \mathrm{~V} \quad \mathrm{~V}_{\mathrm{OSC}}=200 \mathrm{mV} \mathrm{~V}_{\mathrm{RMS}} \\ & \mathrm{~F}=1 \mathrm{MHz} \end{aligned}$ |  | 100 | pF |

THERMAL RESISTANCE

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $R_{\text {th( }(-\mathrm{a})}$ | Junction to ambient |  | 170 |
| ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |  |  |  |

Fig. 8 : TEST CIRCUIT FOR Iswoff PARAMETER : GO - NO GO TEST


This is a GO-NO GO test which allows to confirm the switch-off current (l l ) level in functional test circuit.

## TEST PROCEDURE

- Adjust the current level at the Iswoff value by short circuiting the D.U.T
- Fire the D.U.T with a surge current : Ipp = 10 A, $10 / 1000 \mu \mathrm{~s}$
- The D.U.T will come back to the off-state within a duration of 50 ms max.

Fig. 9 : Typical variation of switching-on current (positive or negative) versus RSENSE resistor and junction temperature (see test condition Fig. 11).


Fig. 11 : Iswon MEASUREMENT

- ISWON = I1 when the CLP30-200B1 switches on (11 is progressively increased using R)
- Both TIP and RING sides of the CLP30-200B1 are checked
$-R L=10 \Omega$.


Fig. 10 : Variation of switching-on current versus RSEnse at $25^{\circ} \mathrm{C}$.

fig. 12 : Relative variation of switching-off current versus junction temperature (for RSENSE between 3 and $10 \Omega$ ).

## Iswoff [Tj ${ }^{\circ} \mathrm{C}$ ] I Iswoff $\left[25^{\circ} \mathrm{C}\right.$ ]



Fig. 13 : Relative variation of switching-off current versus RSENSE (between 3 and $10 \Omega$ ).

Iswoff [Rsense] / Iswoff [4 $\Omega$ ]


Fig. 15 : Relative variation of internal reference voltage versus junction temperature (llG $=1 \mathrm{~mA}$ ).


Fig. 17 : Surge peak current versus overload duration (maximum values).


Fig. 14 : Relative variation of switching-on voltage versus $\mathrm{dV} / \mathrm{dt}$ with an external resistor of $3 \Omega$.


Fig. 16 : Capacitance (TIP/GND) versus applied voltage (typical values).


PACKAGE MECANICAL DATA SO8 plastic


MARKING

| Ordering code | Marking | Package | Weight | Base qty | Delivery mode |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CLP30-200B1 | CLP30 | SO-8 | 0.08 g | 100 | Tube |
| CLP30-200B1RL | CLP30 | SO-8 | 0.08 g | 2500 | Tape \& Reel |

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